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DETERMINATION OF RATE CONSTANTS OF CONSECUTIVE FIRST ORDER REACTIONS OCCURRING ON CHROMATOGRAPHIC COLUMNS

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ABSTRACT

Approximate analytical equations were developed for the products of consecutive reactions occurring on a chromatographic column. The equations were tested both by numerically evaluated chromatograms and the acid catalyzed hydrolysis of phthalic dichloride in a liquid chromatographic reactor.

INTRODUCTION

The determination of rate constants from chromatograms of on-column reacting substances has been reported

several times by different authors /1 /, /2 /.

Mostly, however, the papers are focused on simple first order reactions or do not pay attention to the possibility of the occurrence of complex reactions.

The present paper deals with first order consecutive reactions: $A_1 \xrightarrow{k_1} A_2 \xrightarrow{k_2} A_3$.

It is characteristic for a chromatographic reactor that the separation of reactants and products is incomplete, since the reactions occur from the beginning until the end of the columns, and there is no possibility of a separation of the products formed near the end of the column. Therefore, in consecutive reactions always a mixture of the intermediate product and the final product is observed, and the evaluation of peak shape equations for both substances becomes necessary.

PULSE SHAPE EQUATIONS

Mathematical derivation and semi-analytical solution

The mathematical derivation of the pulse shape equations will be based on the following idea:

While passing a cross-section of the chromatographic column the reactant produces a differential product pulse having the initial shape of the reactant pulse at

this cross-section and an amount of substance due to the kinetics of its formation. This differential product pulse is then eluted in a normal chromatographic way, i. e. the moments of the pulse shape equation are altered in the same way as for an injected substance.

The product pulse at the end of the column is then derived by adding (integrating) all the concentration elements of all differential product pulses, which pass simultaneously at the end of the column. However, in case of an intermediate product of a consecutive reaction one must consider the loss of substance due to its transformation to the final product. Therefore, the amount of a differential pulse from the intermediate product at the end of the column is given by the product of the amount produced at x , which is $m_{10}k_{1a} \exp(-k_{1a} x/l) dx$, and a factor for the part not converted to the final product, which is $\exp(-k_{2a}(l-x)/l)$:

$$dm_2(l) = m_{10}k_{1a} e^{-k_{1a} \frac{x}{l}} e^{-k_{2a} \frac{(l-x)}{l}} dx \quad (1)$$

Hence, a concentration element of the product pulse is given by multiplication of the amount of the product pulse and a pulse shape equation (for a summary of suitable pulse shape equations see /3/):

$$dc_2(x, l, t) = dm_2(x, l) \psi(\mu_i, t) dx \quad (2)$$

The intermediate product pulse shape equation was found by transformation of Eqn.(2) to time coordinates using the equation

$$\frac{x}{l} = \frac{(\mu - \mu_2)}{(\mu_1 - \mu_2)} \quad (3)$$

and integration:

$$c_2 = m_{10} k_1 e^{-k_2(\mu_1 - \mu_2)} e^{-(k_1 - k_2)(t - \mu_2)} \int_{\mu_1}^{\mu_2} e^{-(k_1 - k_2)(\mu - t)} \psi d\mu \quad (4)$$

The derivation of a pulse shape equation for the final product is still more complicated:

First, a differential amount of the final product pulse is considered, which is formed by a differential intermediate product pulse at position y in the column. The differential intermediate product itself was formed before at the position x (with $x < y$):

$$\begin{aligned} ddm_3 &= k_{2a} dm_{20}(x, x) e^{-k_{2a}(\frac{y}{l} - \frac{x}{l})} dy \\ &= m_{10} k_{1a} k_{2a} e^{-(k_{1a} - k_{2a})\frac{x}{l}} e^{-k_{2a}\frac{y}{l}} \end{aligned} \quad (5)$$

Then, multiplication with the pulse shape equation, transformation to time coordinates and integration leads to the final product pulse shape equation:

$$C_3 = m_{10} k_1' k_2'' e^{-\Delta k(t-\mu_2)} e^{-k_2''(t-\mu_3)} \int_{\mu_2}^{\mu_1} e^{-\Delta k(\mu-t)} \int_{\mu_2}^{\mu} e^{-k_2''(\mu-t)} \psi d\mu' d\mu \quad (6)$$

Even in case of the probably simplest single pulse shape equation, the Gaussian, a numerical solution of both the product pulse equations (Eqn. 4 and Eqn. 6) is necessary, since the standard deviation of the differential pulse shapes depends on μ and μ' , respectively.

However, if the standard deviations of the pulses do not differ in order of magnitudes one can apply approximate equations for the standard deviations, in which these do not depend on the μ or μ' , but on the time. In the evaluation of the standard deviation of the final product its dependence on the standard deviation of the intermediate product is completely neglected.

$$\sigma^2 = \sigma^2_i + \frac{t - \mu_i}{\mu_1 - \mu_i} (\sigma^2_1 - \sigma^2_i) \quad (7)$$

intermediate product: $i=2$

final product: $i=3$

Moreover, the approximate formulae developed here lead to slight "losses" or "gains" of mass due to an additional skewness of the product peaks, which is produced by the approximation.

Then, some partial integrations with the final product functions (Eqn.6) are possible, leading to:

$$\begin{aligned}
C_3 = & m_{10} \frac{k_1 k_2''}{\Delta k} e^{-\Delta k(t-\mu_2)} e^{-k_2''(t-\mu_3)} \\
& [PI(\mu_2, \mu_1, (\Delta k + k_2'')) \\
& + e^{-\Delta k(\mu_2-t)} (PI(\mu_3, \mu_2, (k_2'')) \\
& - e^{-\Delta k(\mu_2-t)} e^{-\Delta k \frac{\Delta \mu_{12}}{\Delta \mu_{13}} (t-\mu_3)} PI(\mu_3, \mu_1, (\Delta k \frac{\Delta \mu_{12}}{\Delta \mu_{13}} + k_2''))]
\end{aligned} \tag{8}$$

Similar, Eqn. 3 for the intermediate product can be rewritten:

$$\begin{aligned}
C_2 = & m_{10} k_1 e^{-(k_2(\mu_1-\mu_2))} \\
& e^{-k_2(t-\mu_2)} PI(\mu_1, \mu_2, (k_1 - k_2))
\end{aligned} \tag{9}$$

The product integral PI in Eqn. 8 and Eqn. 9 is defined by:

$$\begin{aligned}
PI(\mu_A, \mu_B, k, \sigma) = & e^{\frac{k}{2}\sigma^2} \\
& \left(\int_{-\infty}^{\mu_B} \frac{1}{\sqrt{2\pi}\sigma} e^{-\left(\frac{t-\mu}{2\sigma}\right)^2} d\mu - \int_{-\infty}^{\mu_A} \frac{1}{\sqrt{2\pi}\sigma} e^{-\left(\frac{t-\mu}{2\sigma}\right)^2} d\mu \right)
\end{aligned} \tag{10}$$

The main advantage of the approximation is that it becomes possible to evaluate approximate product pulses in very short time (using polynomial approximations for the Gaussian integrals /6/), which is favorable for curve fitting procedures - in our opinion the only one possibility to calculate rate constants from reaction chromatograms of complex reactions.

Discussion of the product pulse shapes

First of all it should be pointed out, that the PI-functions in the product pulse equations become one or at least constant between the moments forming the boundaries of the integral.

Therefore, similar to the product pulse in a simple irreversible reaction the intermediate product pulse is an exponential function between μ_1 and μ_2 . However, while in a simple reaction there is always a decay from μ_1 to μ_2 , the intermediate pulse can increase, decrease or even become constant, depending on the sign of the difference between the rate constants (Fig. 1). If there was a possibility to observe the pure intermediate, the difference of the rate constants could be evaluated by the so-called product curve method /4/, /5/.

For the final product pulse there are two different parts (Fig.2). First, the part between the retention time of the final product and the retention time of the intermediate, in which the final product curve has a convex curved shape:

$$C_3 = m_{10} \frac{k_1 k_2''}{\Delta k} e^{-k_2''(t-\mu_3)} \left(1 - e^{\Delta k \frac{\Delta \mu_{12}}{\Delta \mu_{13}} (t-\mu_3)} \right) \quad (11)$$

Second, the part between the retention time of the intermediate and the retention time of the reactant, in

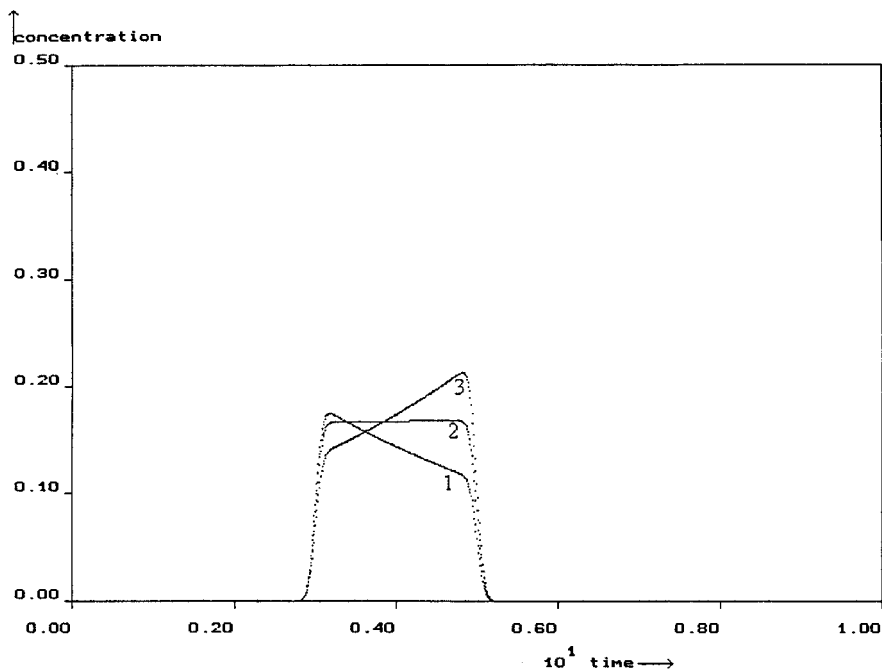


FIGURE 1: INTERMEDIATE PRODUCT PULSE OF A CONSECUTIVE REACTION
(1: $k_1' - k_2' < 0$, 2: $k_1' - k_2' = 0$, 3: $k_1' - k_2' > 0$)

which the final product curve has a concave (almost exponentially decaying) curved shape:

$$C_3 = m_{1.0} \frac{k_1' k_2''}{\Delta k} e^{-k''(\mu_2 - \mu_3)} e^{-(k_1' - k_2')(t - \mu_2)} \left(1 - e^{-\Delta k(\mu_2 - \mu_3)} e^{\Delta k \frac{\Delta \mu_{23}}{\Delta \mu_{13}} (t - \mu_3)} \right) \quad (12)$$

Also, from these equations it can be concluded that the concentration of the final product disappears at μ_1 and

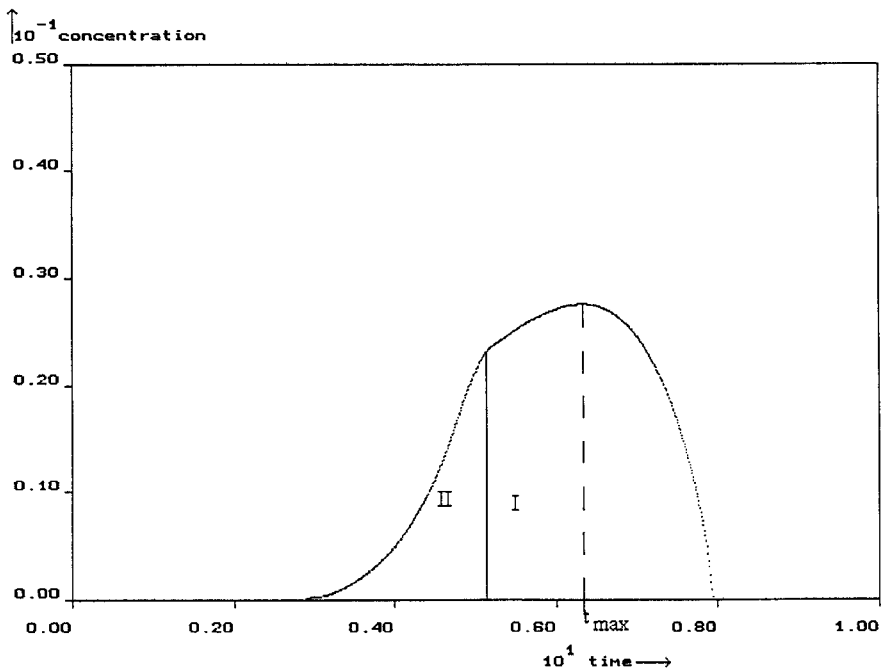


FIGURE 2: FINAL PRODUCT PULSE OF A CONSECUTIVE REACTION (I: CONVEX PART, II: CONCAVE PART)

μ_3 , which is completely in contrast to the intermediate product.

There is a local maximum between μ_3 and μ_2 for the final product. The maximum concentration can be evaluated (diffusion neglected):

$$c_3(t_{\max}) = m_{10} k_1 \frac{\Delta \mu_{12}}{\Delta \mu_{13}} e^{-\Delta k \frac{\Delta \mu_{12}}{\Delta \mu_{13}} (t_{\max} - \mu_3)} \tag{13}$$

It can be seen from Fig.1 and 2 that there is a marked difference between the shape of the final product pulse

and the shape of the intermediate product pulse or the shape of a simple product pulse. As was indicated in a previous publication /5/ there is no marked difference in the shapes of product pulses of parallel reactions, moreover, their shapes are similar to the shape of a simple product pulse. Therefore, the investigation of product pulse shapes might be helpful in investigations of reaction mechanisms.

Results of numerical evaluations

In order to test the possibility to obtain rate constants from reaction chromatograms by fitting the sum of Equations (8) and (9) to the corresponding part of the chromatogram a reaction chromatogram was calculated by an explicit difference method.

Since there are eight parameters in the fitting equation leading to numerous side maxima, the initial values have to be chosen carefully. Fortunately, first approximations for the moments and the standard deviations can be taken from the chromatogram (Fig.3): For the retention times for the reactant and the products from the chromatogram at the maximum of the reactant, the steep flank of the intermediate and the breakthrough point of the final product.

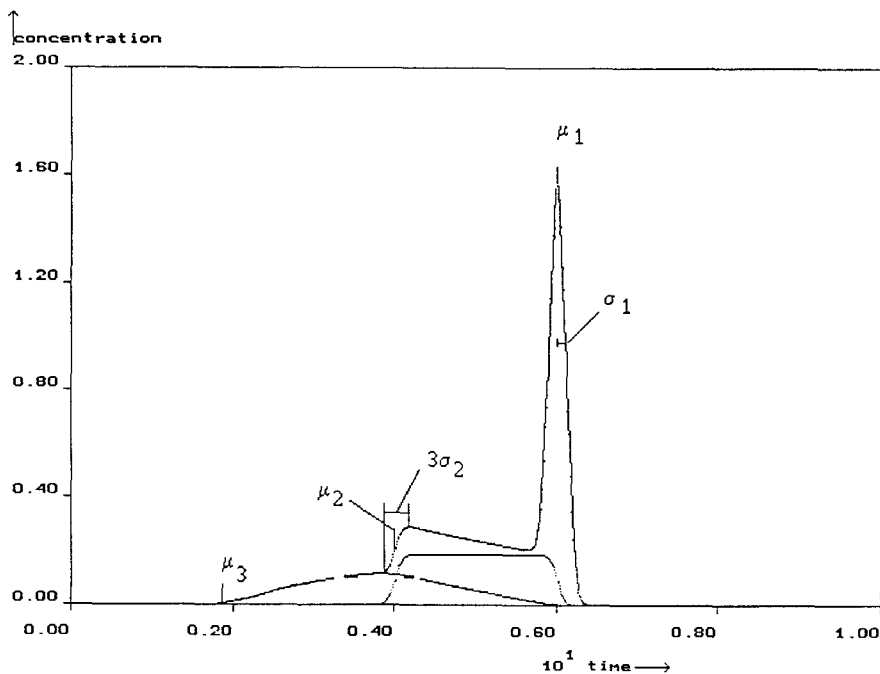


FIGURE 3: INITIAL VALUES FOR THE FITTING CALCULATIONS IN A TYPICAL REACTION CHROMATOGRAM FOR A CONSECUTIVE REACTION

The initial values for the rate constants were established by their systematic variation at the beginning of the fitting procedure.

Fig. 4 shows the excellent agreement between best fit and numerical chromatogram.

Also, as can be seen from Table 1, the parameters from the fitting are in accordance with the parameters given for the numerical calculation of the chromatogram.

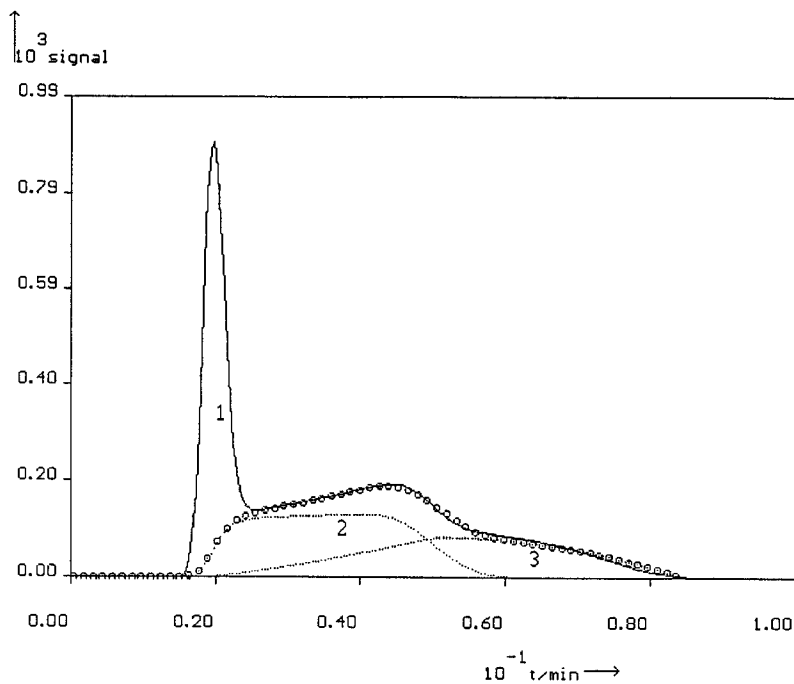


FIGURE 4: PRODUCT CURVE FUNCTIONS (EQN. 8 and EQN. 9) FITTED TO A NUMERICALLY EVALUATED CHROMATOGRAM
(LINE: NUMERICAL EVALUATION, CIRCLES: SUM OF EQN. 8 and EQN. 9 ; 1=REACTANT, 2=INTERMEDIATE, 3=PRODUCT)

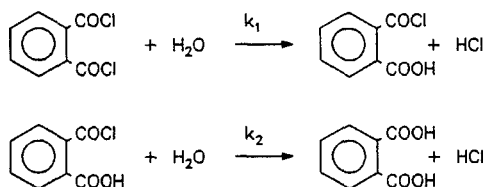
TABLE 1

Results of the Recalculation of the Parameters of a Numerical Chromatogram

	k_1	k_2	μ_1	μ_2	μ_3
num.	1.20	1.20	3.00	5.00	8.00
fitting	1.20	1.17	2.98	4.98	8.02

EXPERIMENTAL

The acid-catalyzed hydrolysis of phthalic dichloride



was investigated using the following liquid chromatographic equipment: A modular HPLC system from Gamma Analysentechnik Berlin, Germany (Kortec K35D HPLC pump, GAT-PHD 601 rapid scan UV-VIS detector with computer interface) with an EnCaPharm 100 RP 18 column from Molnar-Institut Berlin, Germany, which is persistent to high and low pH-ranges /6/ .

Acetonitrile/water (50:50) was the eluent, containing 10^{-2} mol/l HCl as acidic catalyst.

Experiments were carried out at 25°C with flow rates of 1.0 ml/min, 0.5 ml/min, 0.25 ml/min and 0.12 ml/min.

The chromatograms were recorded in the rapid scanning mode of the detector from 200 nm to 320 nm in steps of 1 nm. 0.5 μ l of a 0.07 mol/l solution from phthalic dichloride in acetonitrile were injected.

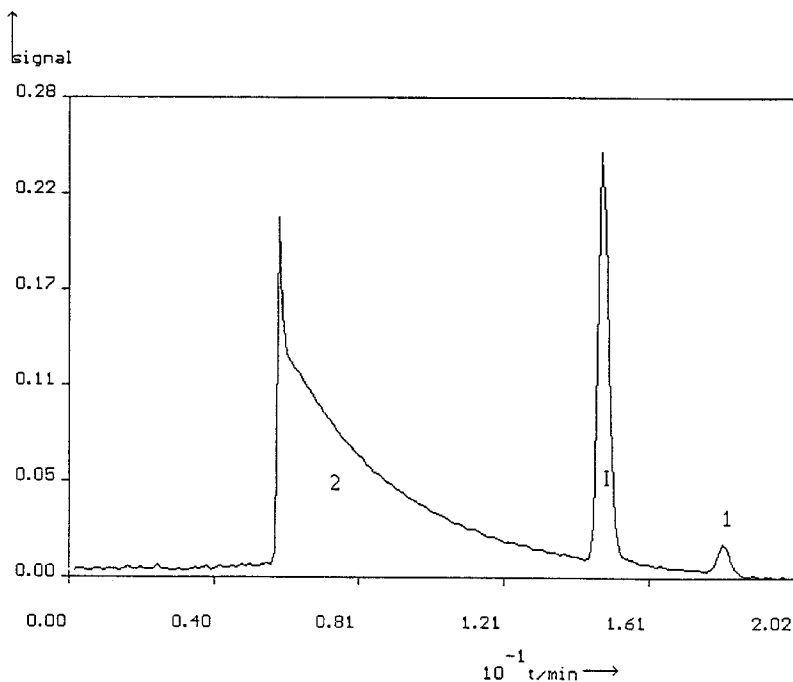


FIGURE 5: REACTION CHROMATOGRAM OF THE HYDROLYSIS OF PHTHALIC DICHLORIDE AT A FLOW RATE OF 1ml/min (1: PHTHALIC DICHLORIDE, 2: PHTHALIC CHLORIDE, I: IMPURITY)

RESULTS AND DISCUSSION

The experimental product curves were fitted by the functions (8) and (9) as shown in Fig. 5 - Fig. 8, considering a different molar detector response:

$$D = f * (c_3 + f_{23} c_2) \quad (14)$$

The detector response ratio of the products f_{23} was ex-

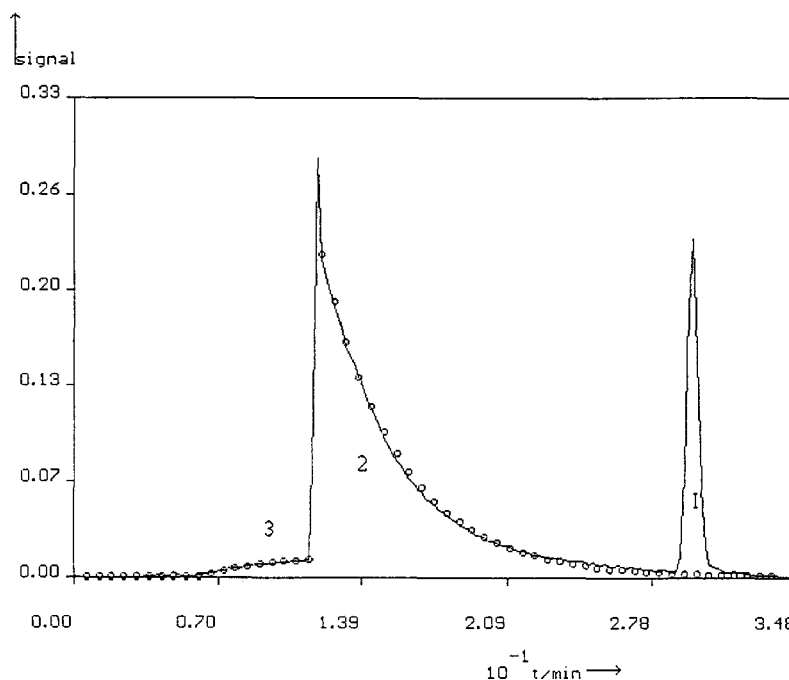


FIGURE 6: BEST FIT OF EQN. 14 TO A REACTION CHROMATOGRAM OF THE HYDROLYSIS OF PHTHALIC DICHLORIDE AT A FLOW RATE OF 0.5ml/min (LINE: EXPERIMENT, CIRCLES: EQN. 14, 2: PHTHALIC CHLORIDE, 3: PHTHALIC ACID, I: IMPURITY)

perimentally determined. In the investigations discussed here there was the problem that conversion for the reactant was already nearly complete, while there was still little final product formed. However, the phthalic chloride contained an inert impurity, the peak of which could be used to establish the reaction duration.

As can be seen from Figures 5-8 there is a good agree-

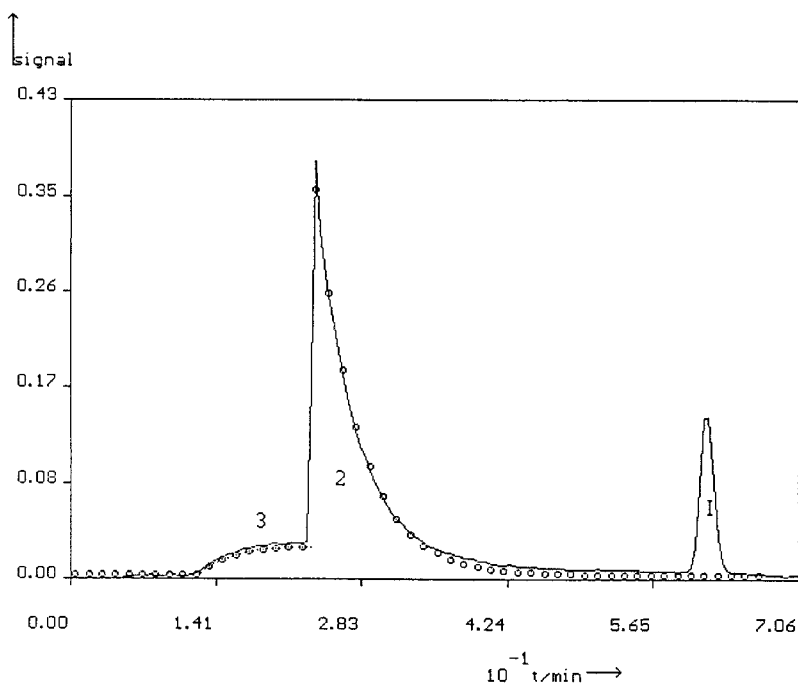


FIGURE 7: BEST FIT OF EQN. 14 TO A REACTION CHROMATOGRAM OF THE HYDROLYSIS OF PHTHALIC DICHLORIDE AT A FLOW RATE OF 0.25ml/min (LINE: EXPERIMENT, CIRCLES: EQN. 14, 2: PHTHALIC CHLORIDE, 3: PHTHALIC ACID, I: IMPURITY)

ment between the experimental results and the product curves calculated from Eqn. (14).

Apparent rate constants were calculated with respect to the retention time of the reactant. These are shown in Table 2.

There is a sufficient agreement between the rate constants of the different runs.

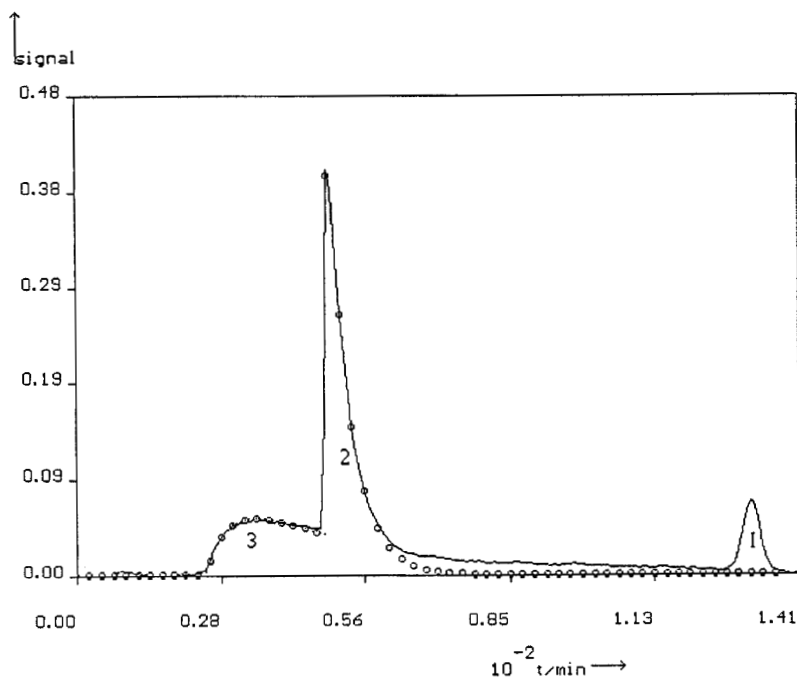


FIGURE 8: BEST FIT OF EQN. 14 TO A REACTION CHROMATOGRAM OF THE HYDROLYSIS OF PHTHALIC DICHLORIDE AT A FLOW RATE OF 0.12ml/min (LINE: EXPERIMENT, CIRCLES: EQN. 14, 2: PHTHALIC CHLORIDE, 3: PHTHALIC ACID, I: IMPURITY)

TABLE 2

Apparent Rate Constants for the Hydrolysis of Phthalic Dichloride as Evaluated from Fitting of Eqn. 14 to Experimental Chromatograms

flow rate	0.5 ml/min	0.25ml/min	0.12ml/min
k_1	0.19/min	0.18/min	0.18/min
k_2	0.0057/min	0.0054/min	0.0053/min

CONCLUSIONS

Especially Equations (8) and (9) show that the intermediate and the final product are eluted together during a considerable time.

The product pulse shape of the intermediate is closely related to the pulse shape of a simple product pulse (exponential decay function). The product pulse shape of the final product consists of a concave and a convex part, and no useful linearization can be found for these parts. Therefore, the determination of rate constants from those reaction chromatograms requires a fitting procedure.

It was found that the sum of equations (8) and (9) can be fitted to numerical chromatograms as well as to experimental chromatograms, and both rate constants were established by this procedure.

SYMBOLS

- D : detector signal
f : response factor
 f_{23} : detector response ratio of intermediate and final product
c : concentration
 k_1' : virtual rate constant, defined by $k_1' = k_{1a} t_0 / (\mu_1 - \mu_2)$

- k_2' : virtual rate constant, defined by $k_2' = k_{1a} t_0 / (\mu_1 - \mu_2)$
 k_2'' : virtual rate constant, defined by $k_2'' = k_{2a} t_0 / (\mu_2 - \mu_3)$
 k_{ia} : apparent rate constant $k_{ia} = k_{i \text{ mobile}} + q_i * k_{i \text{ stationary}}$
 l : length of the column
 m_i : zeroth moment
 m_{i0} : initial zeroth moment of first reactant
 q_i : retention capacity
 t : time
 t_0 : dead time
 x : length coordinate
 y : length coordinate
 Δk : $k_1' - k_2' - k_2''$
 $\Delta \mu_{ij}$: $\mu_i - \mu_j$
 μ_1 : retention time of the reactant
 μ_2 : retention time of the intermediate
 μ_3 : retention time of the final product
 μ_E : $\mu_3 + (\mu - \mu_2) (\mu_1 - \mu_3) / (\mu_1 - \mu_2)$
 μ : integration variable in Eqn. 4
 μ' : integration variable in Eqn. 6
 σ_i : standard deviation
 ψ : pulse shape equation (i.e. Gaussian distribution)

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